#### EVALUATION OF TROPHIC STATUS FOR LAKE HAMILTON

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Submitted in Partial Fulfillment of the Requirmements for the Degree of Master of Science in the School of Engineering Civil Engineering Department

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#### Abstract

EVALUATION OF TROPHIC STATUS FOR LAKE HAMILTON Bassel Abdul-Hakim Abbas Master of Science in Civil Engineering Youngstown State University, 1992

There were two main goals of this project, the first was to evaluate the trophic status of Lake Hamilton, using empirical and simple mechanistic models. The second was to obtain a detailed data base for 1987 that could be used to model eutrophication with a sophisticated model.

Field sampling was performed on 25 dates during 1987; temperature and dissolved oxygen profiles were determined at the sampling sites. Samples were collected and analyzed for soluble reactive phosphorus, total soluble phosphorus, nitrate, ammonia and chlorophyll <u>a</u>.

Many hydrologic and morphometric parameters were calculated for Lake Hamilton. Also, the large amount of data collected for the lake is suitable for future use in more. detailed water quality modeling. Lake Hamilton trophic status was predicted to be eutrophic using Vollenweider's (1975) loading plot. Based on the procedure of Dillon and Rigler (1975), the phosphorus loading to Lake Hamilton was estimated to be 2524 kg/Yr. It was also estimated that a 60%

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reduction in phosphorus loading would be required to improve the lake from a eutrophic to a mesotrophic condition. To my Mother, Father, and Uncle Without your Love, Support, and Encouragement I would not be here. To my dear wife Your Help, Affection, and Understanding

Made this project a simpler task.

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#### Chapter One

#### Introduction

Eutrophication is the natural process of fertilizing surface waters by the input of nutrients (nitrogen and phosphorus); these nutrients will promote algal growth when adequate light is available. Algae will, in turn, settle to the bottom of the basin and die. Aerobic bacteria at the bottom then start working to decompose the dead material, consuming dissolved oxygen. The more nutrients introduced to a lake, the more algae are produced in the epilimnion (upper waters) and the more oxygen is depleted by the bacteria in the hypolimnion (bottom waters). Algal growth causes turbidity that limits light penetration and may limit production to the surface layers of the lake. The depletion of dissolved oxygen by the bacteria may result in anaerobic conditions.

Eventually, enough algae die and fill up the lake, producing what we know as a peat bog. This process takes thousands of years to occur naturally, but can be accomplished in only a decade if enough nutrients are introduced into the lake as a result of human activities. Often the growth-limiting algal nutrient is phosphorus (P), which is introduced from agricultural runoff, detergents, and human or animal waste. The trophic status of lakes is classified into one of three categories:

- Oligotrophic: very low nutrient levels and algal productivity.
- Mesotrophic: moderate nutrient and productivity levels.

3. Eutrophic: high nutrient levels and productivity. Eutrophic conditions make a water undesirable for body contact recreation or use as a drinking water source.

Mathematical models are used to analyze water quality in a lake; these models range from very simple, empirical equations to sets of very complex, theoretical (or "mechanistic") equations that must be solved using numerical techniques. These models can be used to evaluate the adequacy of existing data, determine what processes are most important in lakes, and predict how the lake will respond to changes in external loadings (for example, of P) or environmental conditions. Many different models have been developed to provide insight into the problem of eutrophication.

The focus of this study was Lake Hamilton in Struthers, Ohio (Figure 1.1). This man-made lake was constructed in 1905 by the damming of Yellow Creek, and it is owned by the Ohio Water Service Company. It is currently used as the source of drinking water by the City of Campbell, Ohio. It is also used by several different industries in the area.

There were two main objectives of this study. The first was to evaluate the trophic status of Lake Hamilton, using convenient empirical and mechanistic models. The second was



Figure 1.1 Map Showing Location of Lake Hamilton

to obtain a detailed data base for 1987 that could be used to model eutrophication with a more detailed mechanistic model (such as USEPA's WASP4 program).

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#### Chapter Two

Literature Review

#### 2.1. Basic Concepts of Mathematical Modeling

The goals of this study were to apply some simple models to classify the trophic status of Lake Hamilton, and to develop a data base that could be used in applying more complex models. A mathematical model is defined as an equation or graphical representation describing the relationship(s) between two or more parameters or characteristics in a body of water. There are two types of mathematical models - empirical and deterministic. The empirical models are developed from observations on many different systems (lakes). Examples include: a plot of chlorophyll <u>a</u> versus mean depth by Sakamoto (1966); a regression equation of Secchi depth versus dissolved oxygen (D.O.) deficit by Lasenby (1975); a regression equation of chlorophyll a versus total phosphorus by Dillon and Rigler (1974); and phosphorus loading plots developed by Vollenweider (1968, 1975), to name only a few. Deterministic (or "mechanistic") models are derived from theoretical considerations and equations. A simple deterministic model for total phosphorus (TP) in lakes was proposed by Dillon and Rigler (1974): This model was based on the assumption that

the lake is completely mixed and at steady-state. The model equation is:

$$TP = \frac{La (1-R)}{q_s}$$
(2.1)

where TP = total P concentration,  $g/m^3$ ;

 $L_a$  = areal TP loading rate; g/m<sup>2</sup>/yr;

R = phosphorus retention coefficient, unitless;

q<sub>s</sub> = areal water loading rate, m/yr.

An empirical equation for R was developed by Kirchner and Dillon (1974).

Another similar deterministic model was proposed by Chapra (1975). The model equation is:

$$TP = \underline{La}$$
(2.2)  
$$q_s + v$$

where v = TP settling rate, m/yr. Various values have been proposed for v. Vollenweider (1975) suggested 10.0 m/yr; Dillon and Kirchner (1975) recommended 13.2 m/yr; and Chapra (1975) used a value of 16.0 m/yr.

#### 2.2 Methods Used for Lake Trophic Status Classification:

Phosphorus loading plots are used to predict whether a lake will be oligotrophic, mesotrophic, or eutrophic. The simplest is by Vollenweider (1968), which involves plotting areal TP load versus mean lake depth. A more advanced plot was developed by Vollenweider (1975), which involves plotting areal TP loading versus a real water loading. The plot is divided into three regions corresponding to the different trophic status classifications.

Lake Trophic Status Indices (TSI) are equations or tables used to classify a lake according to its trophic status based on experimental observations. There are several different methods for calculating (TSI). Examples include Shannon and Brezonik (1972), and Carlson (1977). The latter is based on average values of TP, Secchi depth, and chlorophyll <u>a</u>. Walker (1979) proposed an averaged modification of Carlson's equations.

Dillon and Rigler (1975) developed a simple procedure for evaluating the trophic status of a lake and capacity to withstand additional development based on phosphorus loading, morphometry and hydrology. This "desk method" requires a minimum of field data, and combines several empirical models with the simple TP model of Dillon and Rigler (1975); i.e., equation 2.1.

#### Chapter Three

#### Methods and Procedures

#### 3.1 Field Work

Field sampling was performed on 25 dates during 1987. A deep water site (Figure 3.1) was visited on all dates; a shallow site was visited on only four dates. Grab samples were also obtained by hand from Yellow Creek upstream or downstream of Lake Hamilton on most sampling dates. Temperature and dissolved oxygen profiles were determined at the sampling sites, using a Yellow Springs Model 57 dissolved oxygen meter. Dissolved oxygen profiles were checked by comparison with measurements made using the Azide Modification of the Winkler method (APHA, 1985) at two depths, and adjusted if necessary. Samples were collected from four depths (usually 1, 4, 8, and 12 m) using a Wildco Alpha Bottle, and the water column transparency was measured using a standard 20 cm diameter Secchi disk attached to a rope with 0.1 meter increments marked on it.

#### 3.2 Lab Preparation

Upon return to the YSU Environmental Engineering Lab, a portion of each water sample was filtered through a 0.45  $\mu$ m pore size membrane. This filtrate was used for the soluble

reactive phosphorus (SRP), total soluble phosphorus (TSP), nitrate and ammonia tests. Filtrations for the chlorophyll <u>a</u> test were performed on the day of sampling using Fisher GF/C glass fiber filters (effective pore size 1.0  $\mu$ m). Unfiltered water was saved for the total phosphorus (TP) test. All samples were stored in the dark at 4°C until the analyses were performed.

#### 3.3 Lab Analysis

All methods used for analysis are according to "Standard Methods" (APHA, 1985), except ammonia (Lind, 1985). Total phosphorus and total soluble phosphorus were measured using the persulfate digestion method. Then the phosphorus measurements were done using the ascorbic acid method. Chlorophyll <u>a</u> concentrations were measured for all samples using the spectrophotometric method. These measurements were done on a Bausch and Lomb Model 1001 spectrophotometer. The nitrate and ammonia analyses were performed by the YSU Biology Department. The nitrate measurements were done using the cadmium reduction method and ammonia measurements were done using the phenate method.



Figure 3.1 Location of Sampling Sites, 1987

#### Chapter Four

#### Results and Discussions

#### 4.1 Morphometry and Hydrology:

Several parameters describing the morphometry and hydrology of the lake were calculated in this study and should be useful in future studies on this lake. Using a planimeter, the areas enclosed by 10 ft. depth contours were measured. The lake basin was divided into a shallow region and a deep region, as shown by the dashed line in Figure 3.1. The area versus depth data is presented in Table 4.1.

A number of important hydrologic and morphometric parameters for Lake Hamilton are summarized in Table 4.2. Although details of some of these calculations are presented later, the values are also listed here to give the reader a feel for the physical characteristics of Lake Hamilton. Details of the water budget calculations are given in Table 4.3. A summary is shown in Figure 4.1.

#### 4.2 Summary of Field Data:

All data obtained during 1987 is tabulated in Tables 4.4 through 4.13. Volume-weighted average concentrations calculated by Kotwal (1992) are presented in Table 4.14. Plots of representative profiles (Parameters versus depth) from the 1987 Lake Hamilton field data are presented for temperature in Figure 4.2, dissolved oxygen in Figure 4.3,

and soluble reactive phosphorus in Figure 4.4. In addition, a plot of Secchi depth versus time is shown in Figure 4.5.

Temperature profiles show that the Lake is thermally stratified in the summer, and the temperature gradient causes resistance to mixing between top and bottom waters. Dissolved oxygen profiles show severe anaerobic conditions during the summer. Soluble Reactive Phosphorus profiles show low levels when the lake water contains oxygen, and show large releases when lake bottom water becomes anoxic during the summer. Secchi Depth profiles show dramatic fluctuations during the year, and that is due to the change in algal species in the lake. Table 4.1 Area Versus Depth for Lake Hamilton

## A. <u>Segment #I</u> - Shallow Region

Area

Area

Depth (ft)	(Acres)	$(\underline{ft}^2)$
0	55.539	2,419,244
10	42.847	1,866,410
20	17.996	783,889
25' (7.62m)	. 0	0

B. <u>Segment II & III</u> - Deep Region

Depth (ft)	(Acres)	( <u>ft</u> <sup>2</sup> )
0	42.600	1,855,663
10	40.934	1,783,123
20 (6.1 m)	36.223	1,577,903
30	26.951	1,173,972
40	10.295	448,467
50	3.06	133,300
55 (16.76 m)	0	0

Table 4.2 Lake Hamilton Morphometry and Hydrology

Lake Volume =  $V_{Lake}$  = 2.750 x 10<sup>6</sup> m<sup>3</sup> Total Outflow =  $Q_{out}$  = 2.53 x 10<sup>7</sup> m<sup>3</sup>/yr (excluding evaporation) Lake Surf. Area =  $A_0$  = 3.971 x 10<sup>5</sup> m<sup>2</sup> Lake Drainage Area =  $A_d$  = 2.519 x 10<sup>6</sup> m<sup>2</sup> Mean depth = Z = <u>Vol</u>. = 6.90 m Surf Area

Hydraulic Retention Time = t =  $\frac{\text{Vol.m}^3}{\text{Q out, m}^3/\text{yr}}$  = 0.11 yr. = 40 days

Flushing Rate =  $\rho$  = 9.13/yr.

Table 4.3 Water Budget for Lake Hamilton

Outflows (MG) - Data from Ohio Water Service

	<u>1983 1984</u>	<u>1985</u>	<u>1986 1987</u>	Ave 83,84,86,87
Withdrawals	1764 1007	736	995 386	1038
Over Spillway	<u>4551 5403</u>	16979	<u>6871 5764</u>	5647
Total	6315 6410	17715	7866 6150	6685

Ave Total = 6685 MG/yr =  $2.53 \times 10^7 \text{ m}^3/\text{yr}$ Withdrawals -  $3.93 \times 10^6 \text{ m}^3/\text{yr}$ Over Spillway -  $2.14 \times 10^7 \text{ m}^3/\text{yr}$  (excluding 1985)

Direct Precipitation:

Mean Annual Rainfall = 37.90 in. (NOAA, 1982) = 0.9627 m/yrLake Surface Area =  $3.972 \times 10^5 \text{ m}^2$ 

Direct precip. =  $(3.972 \times 10^5 \text{ m}^2)(0.9627 \text{ m/yr})$ 

 $= 3.82 \times 10^5 \text{ m}^3/\text{yr}$ 

Direct Runoff

Runoff coefficients (Viessman, et al, 1989):

Residential:  $0.32 = C_1$ 

Unimproved:  $0.20 = C_2$ 

Watershed areas:

Residential: 1,967,022  $m^2 = A_1$ 

Unimproved: 551,702  $m^2 = A_2$ 

Direct Runoff = Rainfall x  $(C_1A_1 + C_2A_2)$ 

 $= 712,193 \text{ m}^3/\text{yr} = 7.12 \text{ x} 10^5 \text{ m}^3/\text{yr}$ 

Evaporation = 31 in/yr (Linsley, et al, 1992) = 0.787 m/yr

Table 4.3 (continued)

Evaporation Loss =  $0.787 \text{ m x} (3.972 \text{ x} 10^5 \text{ m}^2)$ =  $3.13 \text{ x} 10^5 \text{ m}^3/\text{yr}$ 

Yellow Creek Total Direct Direct Direct Inflow = Outflow + Evaporation - Precip. - Runoff =  $2.53 \times 10^7 + 3.13 \times 10^5 - 3.82 \times 10^5 - 7.12 \times 10^5$ m<sup>3</sup>/yr

 $Q_{in} = 2.45 \times 10^7 \text{ m}^3/\text{yr}$ 





<u>Depth (m)</u>	<u>3/27</u>	4/9	4/23	4/30	5/08	5/15	5/21	5/28	6/04	6/12
0.5	7.9	5.9	17.4	9.8	13.0	18.0	17.3	22.0	23.0	21.1
1.0	7.8	5.8	17.3	9.8	13.0	17.6	17.3	21.9	23.0	21.1
1.5	7.8	5.8	14.5	10.0	12.8	17.4	17.3	21.8	23.0	21.0
2.0	7.7	5.1	10.5	10.0	11.4	16.8	17.3	19.8	22.6	21.2
2.5	7.5	4.6	9.5	10.0	10.8	16.2	17.3	18.7	21.2	21.1
3.0	7.3	4.1	9.0	10.0	10.4	15.2	15.0	17.1	19.0	20.9
3.5	7.2	4.0	8.3	9.8	10.0	13.5	13.0	15.5	16.8	20.0
4.0	6.0	3.8	7.4	9.5	9.7	10.5	11.2	13.1	14.0	17.9
4.5	5.7	3.8	6.5	9.3	8.5	9.6	10.1	11.1	12.2	14.5
5.0	5.3	3.8	6.0	7.8	7.8	8.7	9.1	9.5	10.5	12.1
5.5	5.2	3.8	5.8	7.0	6.9	8.3	8.2	8.3	9.0	10.6
6.0	4.9	3.8	5.4	6.0	5.9	7.5	7.5	7.6	8.2	9.5
7.0	3.5	3.9	4.9	5.2	5.2	6.0	6.0	6.0	6.5	7.0
7.5	2.9	3.9	4.8	5.0	4.9	5.5	5.6	5.7	6.0	6.1
8.0	2.7	3.8	4.4	4.8	4.5	5.1	5.2	5.2	5.5	5.9
8.5	2.1	3.7	4.0	4.4	4.5	4.7	5.1	5.0	5.2	5.1
9.0	2.0	3.4	3.9	4.0	4.2	4.5	4.8	4.7	4.8	4.9
9.5	2.0	3.1	3.9	3.8	3.9	4.3	4.5	4.5	4.7	4.8
10.0	2.0	2.8	3.9	3.6	3.8	4.2	4.2	4.3	4.4	4.5
10.5	2.0	2.3	3.4	3.5	3.6	4.0	4.0	4.2	4.3	4.4
11.0	2.0	2.2	3.0	3.3	3.5	3.8	3.9	4.0	4.2	4.3
11.5	2.0	2.2	3.0	3.3	3.4	3.5	3.8	4.0	4.0	4.1
12.0	2.0	2.5	3.0	3.0	3.3	3.5	3.6	3.8	4.0	4.1
12.5	2.0	2.5	2.9	3.0	3.2	3.4	3.5		4.0	4.1
13.0	2.0	2.5	2.9	3.0	3.2	3.4	3.5		3.8	4.1
13.5		2.6	2.9	2.9		3.4				4.1
14.0			3.0							

## Table 4.4. (Continued)

### Temperature (°C)

Ľ	epth	(m)	6/17	6/23	7/02	7/07	7/14	7/21	7/27	8/04	8/10	8/21
	0.5		23.8	24.3	21.5	23.4	25.2	26.2	26.3	25.5	23.5	23.9
	1.0		23.8	24.3	21.5	23.4	25.2	26.2	26.1	25.2	23.5	23.9
	1.5		23.8	24.3	21.5	23.4	25.2	26.0	26.0	25.2	23.5	23.9
	2.0		22.5	24.3	21.5	22.3	24.4	25.2	26.0	25.1	23.5	23.9
	2.5		21.5	23.5	21.3	20.7	22.8	24.3	26.0	24.8	23.2	23.9
	3.0		20.9	21.8	20.0	19.9	21.5	22.8	24.4	24.6	22.8	23.8
	3.5		19.8	20.5	19.6	19.5	20.5	21.5	22.0	22.7	22.4	23.0
	4.0		17.1	19.0	19.3	19.1	19.5	19.8	20.7	22.0	22.2	22.0
	4.5		15.7	17.0	19.3	18.0	18.5	19.0	19.2	20.5	20.3	20.9
	5.0		13.1	14.0	18.0	18.0	17.5	17.4	18.0	18.5	18.5	17.2
	5.5		11.5	12.2	14.5	15.5	16.0	15.8	16.2	16.5	17.1	15.8
	6.0		9.9	10.6	13.0	12.0	13.0	14.0	15.6	15.1	15.8	13.7
	6.5		8.8	9.0	11.0	10.5	11.2	12.2	13.0	13.0	13.7	12.4
	7.0		7.5	7.8	9.5	9.0	9.6	10.5	10.8	11.7	12.2	11.1
	7.5		6.9	7.0	8.3	7.9	8.2	8.8	9.2	10.5	10.7	12.8
	8.0		6.2	6.5	7.6	7.2	7.5	8.0	8.2	9.0	9.3	11.5
	8.5		5.8	5.8	6.5	6.4	6.8	7.2	7.0	8.2	7.8	9.5
	9.0		5.4	5.5	6.0	5.8	6.0	6.5	6.7	7.5	7.2	8.5
	9.5		5.1	5.2	5.6	5.5	5.8	6.0	6.1	6.7	6.8	7.6
	10.0		4.8	5.0	5.2	5.2	5.4	5.7	5.9	6.1	6.3	7.1
	10.5		4.8	4.7	5.0	5.1	5.3	5.5	5.7	5.8	6.0	6.5
	11.0		4.5	4.5	4.7	4.9	5.2	5.4	5.4	5.5	5.8	6.1
	11.5		4.5	4.5	4.6	4.7	5.0	5.2	5.2	5.4	5.5	6.0
	12.0		4.4	4.5	4.5	4.7	4.8	5.2	5.0	5.2	5.3	5.8
	12.5		4.2	4.5	4.5	4.5	4.8	5.0	5.0	5.1	5.2	5.5
	13.0		4.1	4.3	4.5	4.5		5.0	5.0	5.0	5.1	5.3
	13.5		4.1	4.3	4.5	4.5		4.8		5.0	5.0	5.2
	14.0											5.2

# Table 4.4. (Continued)

Temperature (°C)

$\begin{array}{cccccccccccccccccccccccccccccccccccc$	<u>Depth (m)</u>	9/01	9/16	9/30	10/16	11/06
1.0 $19.0$ $18.9$ $16.8$ $10.9$ $8.$ $1.5$ $19.0$ $18.7$ $16.8$ $10.9$ $8.$ $2.0$ $19.0$ $18.6$ $16.8$ $10.8$ $8.$ $2.5$ $18.9$ $18.1$ $16.8$ $10.6$ $8.$ $3.0$ $18.8$ $17.8$ $16.8$ $10.6$ $8.$ $3.5$ $18.8$ $17.4$ $16.8$ $10.6$ $8.$ $4.0$ $18.8$ $17.4$ $16.5$ $10.6$ $8.$ $4.5$ $18.7$ $17.2$ $16.2$ $10.6$ $8.$ $4.5$ $18.5$ $17.0$ $16.1$ $10.5$ $8.$ $5.0$ $18.5$ $17.0$ $16.1$ $10.5$ $8.$ $5.5$ $17.3$ $16.7$ $16.0$ $10.5$ $8.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $12.0$ $5.9$	0.5	19.0	18.9	16.9	11.0	8.5
1.5 $19.0$ $18.7$ $16.8$ $10.9$ $8.$ $2.0$ $19.0$ $18.6$ $16.8$ $10.8$ $8.$ $2.5$ $18.9$ $18.1$ $16.8$ $10.6$ $8.$ $3.0$ $18.8$ $17.8$ $16.8$ $10.6$ $8.$ $3.5$ $18.8$ $17.4$ $16.8$ $10.6$ $8.$ $4.0$ $18.8$ $17.4$ $16.5$ $10.6$ $8.$ $4.0$ $18.8$ $17.4$ $16.5$ $10.6$ $8.$ $4.5$ $18.7$ $17.2$ $16.2$ $10.6$ $8.$ $5.0$ $18.5$ $17.0$ $16.1$ $10.5$ $8.$ $5.5$ $17.3$ $16.7$ $16.0$ $10.5$ $8.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$	1.0	19.0	18.9	16.8	10.9	8.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	1.5	19.0	18.7	16.8	10.9	8.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.0	19.0	18.6	16.8	10.8	8.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	2.5	18.9	18.1	16.8	10.6	8.2
3.5 $18.8$ $17.4$ $16.8$ $10.6$ $8.$ $4.0$ $18.8$ $17.4$ $16.5$ $10.6$ $8.$ $4.5$ $18.7$ $17.2$ $16.2$ $10.6$ $8.$ $5.0$ $18.5$ $17.0$ $16.1$ $10.5$ $8.$ $5.5$ $17.3$ $16.7$ $16.0$ $10.5$ $8.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.6$ $5.9$	3.0	18.8	17.8	16.8	10.8	8.2
4.0 $18.8$ $17.4$ $16.5$ $10.6$ $8.$ $4.5$ $18.7$ $17.2$ $16.2$ $10.6$ $8.$ $5.0$ $18.5$ $17.0$ $16.1$ $10.5$ $8.$ $5.5$ $17.3$ $16.7$ $16.0$ $10.5$ $8.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.5$ $5.3$ $5.8$ $5.8$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$ $7.$	3.5	18.8	17.4	16.8	10.6	8.2
4.5 $18.7$ $17.2$ $16.2$ $10.6$ $0.5$ $5.0$ $18.5$ $17.0$ $16.1$ $10.5$ $8.$ $5.5$ $17.3$ $16.7$ $16.0$ $10.5$ $8.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.2$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $7.$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$ $7.$	4.0	18.8	17.4	16.5	10.6	0.2
5.0 $18.5$ $17.0$ $16.1$ $10.5$ $6.$ $5.5$ $17.3$ $16.7$ $16.0$ $10.5$ $8.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.6$ $5.8$ $7.$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$ $7.$	4.5	18.7	17.2	16.2	10.6	0.2
5.5 $17.3$ $16.7$ $16.0$ $10.5$ $6.$ $6.0$ $16.4$ $16.2$ $15.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $7.$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$ $7.$	5.0	18.5	17.0	16.1	10.5	0.2
6.0 $16.4$ $16.2$ $13.9$ $10.5$ $8.$ $6.5$ $15.1$ $15.7$ $15.3$ $10.5$ $8.$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $5.8$ $6.5$ $7.$ $14.5$ $7.$ $7.$ $7.$ $7.$	5.5	17.3	16.7	16.0	10.5	9.2
6.5 $15.1$ $15.7$ $15.3$ $10.5$ $0.5$ $7.0$ $13.3$ $14.7$ $15.2$ $10.5$ $8.$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $5.8$ $6.5$ $7.$ $14.5$ $7.$ $7.$ $7.$ $7.$	6.0	16.4	10.2	15.9	10.5	8.2
7.0 $13.3$ $14.7$ $15.2$ $10.5$ $3.7$ $7.5$ $12.1$ $13.5$ $14.5$ $10.5$ $8.$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $7.$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$	6.5	12.1	13.7	15.5	10.5	8 2
7.5 $12.1$ $13.3$ $14.3$ $10.3$ $0.3$ $8.0$ $11.1$ $12.0$ $13.0$ $10.2$ $8.$ $8.5$ $9.8$ $11.0$ $11.8$ $10.1$ $8.$ $9.0$ $8.9$ $9.8$ $10.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $7.$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$	7.0	13.3	13 5	14.5	10.5	8 2
3.5 $9.8$ $11.0$ $12.0$ $15.0$ $10.2$ $3.1$ $9.0$ $8.9$ $9.8$ $11.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.$ $11.5$ $6.2$ $6.6$ $7.0$ $8.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.$ $12.5$ $5.7$ $6.1$ $6.5$ $7.2$ $8.$ $13.0$ $5.6$ $5.9$ $6.2$ $7.0$ $7.$ $13.5$ $5.3$ $5.8$ $5.8$ $6.5$ $7.$ $14.0$ $5.8$ $7.$ $7.$ $7.$ $14.5$ $7.$ $7.$ $7.$	7.5	12.1	12.0	13 0	10.3	8.2
0.0 $8.9$ $9.8$ $10.0$ $10.1$ $8.9$ $9.5$ $7.8$ $8.4$ $9.8$ $10.1$ $8.9$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.10.1$ $10.0$ $7.2$ $7.9$ $8.5$ $9.9$ $8.10.1$ $10.5$ $6.8$ $7.3$ $7.9$ $9.2$ $8.10.1$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.10.1$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.10.1$ $11.0$ $6.5$ $6.9$ $7.0$ $8.6$ $8.10.1$ $11.5$ $6.2$ $6.6$ $7.0$ $8.0$ $8.10.1$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.10.10.1$ $12.0$ $5.9$ $6.3$ $6.8$ $7.6$ $8.10.10.10.10.10.10.10.10.10.10.10.10.10.$	8.0	9.8	11 0	11 8	10.1	8.2
9.57.88.49.810.18.10.07.27.98.59.98.10.56.87.37.99.28.11.06.56.97.08.68.11.56.26.67.08.08.12.05.96.36.87.68.12.55.76.16.57.28.13.05.65.96.27.07.13.55.35.85.86.57.14.05.87.7.15.07.7.	9.0	8 9	9.8	10.8	10.1	8.2
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	9.5	7.8	8.4	9.8	10.1	8.2
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.0	7.2	7.9	8.5	9.9	8.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	10.5	6.8	7.3	7.9	9.2	8.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	11.0	6.5	6.9	7.0	8.6	8.1
$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	11.5	6.2	6.6	7.0	8.0	8.1
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	12.0	5.9	6.3	6.8	7.6	8.1
13.0       5.6       5.9       6.2       7.0       7.         13.5       5.3       5.8       5.8       6.5       7.         14.0       5.8       7.       7.       7.         14.5       7.0       7.       7.         15.0       7.       7.       7.	12.5	5.7	6.1	6.5	7.2	8.0
13.5     5.3     5.8     5.8     6.5     7.       14.0     5.8     7.       14.5     7.     7.       15.0     7.     7.	13.0	5.6	5.9	6.2	7.0	7.9
14.0       5.8       7.         14.5       7.       7.         15.0       7.       7.	13.5	5.3	5.8	5.8	6.5	7.9
14.5 15.0 7.	14.0			5.8		7.9
15.0 7.	14.5					7.6
	15.0					7.6

Table 4.5. Dissolved Oxygen (mg/L) Profiles for Lake Hamilton,

Depth (m)	3/27 4/9	4/23 4	1/30	5/08	5/15	5/21	5/28	6/04	6/12
0.5	14.4 12.8	15.9 1	12.2	15.4	13.3	9.5	10.1	9.3	11.5
1.0	14.1 12.5	16.3 1	12.0	15.3	13.5	9.3	9.8	9.2	10.9
1.5	14.1 12.4	18.6 1	11.8	15.0	13.5	9.2	9.7	9.1	10.6
2.0	13.9 12.1	15.4 1	11.7	14.4	13.5	9.2	9.6	8.4	10.7
2.5	13.9 11.6	13.8 1	11.6	11.5	13.3	9.1	8.6	7.1	10.5
3.0	13.7 11.4	11.6 1	11.4	10.0	12.9	11.1	9.5	7.3	10.3
3.5	13.3 11.2	10.5 1	1.3	9.1	11.8	11.7	12.2	8.8	9.6
4.0	12.7 10.9	9.0 1	1.1	7.8	5.0	7.6	13.6	12.8	7.6
4.5	12.5 10.7	8.6 1	0.2	6.8	2.2	2.7	10.4	13.5	10.2
5.0	12.3 10.6	8.2	8.3	5.4	1.9	1.4	0.6	10.1	13.2
5.5	12.2 10.4	8.1	7.3	5.0	1.7	1.4	0.4	1.5	13.4
6.0	12. 10.4	8.2	6.8	4.7	1.6	1.5	0.4	1.4	2.1
6.5	11.9 10.3	8.0	6.7	5.0	2.1	1.7	0.6	1.4	1.1
7.0	11.4 10.2	8.1	6.8	5.4	2.5	2.0	0.9	1.5	0.9
7.5	10.0 10.2	7.6	6.8	5.7	3.0	2.6	1.5	1.1	0.8
8.0	9.2 9.7	7.8	6.8	5.9	3.7	2.8	1.8	1.4	0.6
8.5	8.7 8.5	7.3	6.7	5.8	3.7	2.8	1.8	1.8	1.0
9.0	8.4 8.2	7.0	6.6	5.8	3.5	3.3	1.9	1.7	1.1
9.5	8.1 7.6	6.6	5.8	5.5	3.5	3.0	2.2	1.4	1.3
10.0	7.4 6.7	5.5	5.3	4.9	3.5	3.9	2.2	1.9	1.3
10.5	7.2 7.1	6.3	4.7	4.1	3.5	2.4	1.9	1.5	0.2
11.0	6.8 7.0	5.6	4.2	5.0	2.8	2.0	0.9	0.9	0.1
11.5	6.4 6.6	5.1	4.8	3.5	1.8	1.4	0.5	0.4	0.0
12.0	5.8 5.8	4.8	3.9	3.0	1.3	0.9	0.0	0.3	0.0
12.5	5.6 5.2	4.1	4.0	2.7	0.5	0.5		0.3	0.0
13.0	4.7 4.8	4.0	3.8	2.5	0.3	0.5		0.3	0.0
13.5	4.5	3.6		1.7	0.3				0.0
14.0									

# Table 4.5. (Continued)

1.0       12.6       11.3       8.6       17.2       11.6       9.1       10.6       15.1       9.6         1.5       12.1       11.1       8.1       17.4       11.5       9.3       10.5       15.1       9.5         2.0       10.9       10.9       7.9       10.3       8.8       10.4       10.3       14.9       8.5	10.3 10.2 10.2 9.8 9.0 0.9 0.7 0.0
1.5       12.1       11.1       8.1       17.4       11.5       9.3       10.5       15.1       9.5         2.0       10.9       10.9       7.9       10.3       8.8       10.4       10.3       14.9       8.5	10.2 10.2 9.8 9.0 0.9 0.7 0.0
2.0  10.9  10.9  7.9  10.3  8.8  10.4  10.3  14.9  8.3	9.8 9.0 0.9 0.7 0.0
	9.0 0.9 0.7 0.0
3.0 7.1 4.9 5.2 4.1 3.8 7.7 11.5 13.5 1.0	0.9 0.7 0.0
3.5 5.3 2.9 5.0 3.8 1.9 6.4 11.7 2.8 0.7	0.7
4.0 5.1 2.7 5.1 3.3 0.0 0.3 0.9 0.0 0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0 0
5.0 11.2 9.9 2.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0
6.0 6.4 7.4 7.0 4.6 2.4 0.3 0.0 0.0 0.0	0.0
6.5 0.4 0.1 4.3 0.1 0.0 0.0 0.0 0.0 0.0	0.0
7.0 0.4 0.0 0.2 0.1 0.0 0.0 0.0 0.0 0.0	0.0
	0.0
8.5 0.4 0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0 0.0	0.0
9.0 0.4 0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0	0.0
9.5 0.4 0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0
10.5   0.4   0.0   0.1   0.0	0.0
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	0.0
12.0 0.4 0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0	0.0
12.5 0.4 0.0 0.1 0.0 0.0 0.0 0.0 0.0 0.0	0.0
	0.0
14.0	0.0

Dissolved Oxygen (mg/L)

# Table 4.5. (Continued)

Dissolved Oxygen (mg/L)

Depth (m)	9/01	9/16	9/30	10/16	11/06
0.5	8.7	14.3	12.8	10.6	
1.0	8.6	14.1	12.7	10.3	11.3
1.5	8.5	13.8	12.7	10.4	
2 0	8.5	8.4	12.6	10.0	
2 5	8.5	5.3	12.2	8.4	
3.0	8 4	2 2	12.3	8.3	10.6
3.5	8 3	2 0	10.9	8.0	
	7 6	2 2	7 9	8.0	
4.0	7 1	1 8	6.8	8.5	
4.5	0.7	1 1	5.4	8.6	
5.0	0.7	0.0	1 6	8 7	
5.5	0.0	0.0	4.0	8 6	10 4
6.0	0.0	0.0	5.7	8 6	10.1
6.5	0.0	0.0	0.9	0.0	
7.0	0.0	0.0	0.2	0.0	
7.5	0.0	0.0	0.1	0.0	
8.0	0.0	0.0	0.0	0.1	
8.5	0.0	0.0	0.0	8.3	0 5
9.0	0.0	0.0	0.0	5.7	9.5
10.0	0.0	0.0	0.0	3.2	
10.5	0.0	0.0	0.0	0.0	
11.5	0.0	0.0	0.0	0.0	
12.0	0.0	0.0	0.0	0.0	10.1
13.0	0.0	0.0	0.0	0.0	
14.0			0.0		9.8

Table 4.6. Secchi Depth (m) for Lake Hamilton, 1987

Date	Depth
03/27 04/09 04/23 04/30 05/08	0.9 0.7 0.9 1.1
05/15	-
05/21	3.7
05/28	4.7
06/04	5.3
06/12	4.1
06/17	4.6
06/23	1.8
07/02	1.0
07/07	1.1
07/14	2.6
07/21	2.9
07/27	2.1
08/04	1.4
08/10	1.3
08/21	2.2
09/16 09/30 10/16 11/06	1.7 1.7 2.1

Table 4.7. Soluble Reactive Phosphorus ( $\mu$ g/L) in Lake Hamilton, 1987:

Depth (m)	3/27	4/09	4/23	4/30	5/08	5/15	5/21	5/28
1.0 4.0 5.0 6.0 8.0 12.0 outlet inlet	4.6 - 2.5 1.4 2.8	3.8 - 1.6 - 1.4 1.9	2.7 2.0 1.7 1.9	3.8 2.8 2.8 2.8 2.8 2.7	2.0 1.6  1.7 8.7  2.4	2.5 1.7 - 1.6 12.6 11.4	5.4 1.7 - 2.7 30.1 - 6.2	6.3 4.8 - 8.4 52.0 51.6
<u>Depth (m)</u>	6/04	6/12	6/17	6/23	7/02	7/07	7/14	7/21
1.0 4.0 8.0 12.0 outlet inlet	3.3 3.3 3.6 107.1 7.3	4.1 1.9 2.7 150.5 - 36.8	4.0 2.4 1.9 194.8 39.5 58.7	3.7 2.3 32.9 178.8 2.1 105.7	2.8 7.1 5.5 65.6 - 64.8	9.9 6.1 32.4 210.1 10.6 17.7	2.9 1.3 31.0 513.4 3.9 62.7	3.0 1.1 55.9 542.5 7.9 15.5
<u>Depth (m)</u>	7/27	8/04	8/10	8/21	9/01	<u>9/16</u>	<u>9/30</u>	10/16
1.0 4.0 8.0 12.0 outlet inlet	1.3 0.2 72.6 532.1 8.1 14.2	1.5 2.1 52.2 578.0 1.7 21.2	3.9 4.8 88.9 458.9 4.2 24.2	0.0 0.0 136.4 516.0 8.3 31.5	$0.0 \\ 0.0 \\ 214.7 \\ 123.2 \\ 1.4 \\ 31.7$	1.0 0.5 128.3 562.8 0.9 19.7	$ \begin{array}{r} 1.7\\ 0.4\\ 0.5\\ 654.7\\ 41.8\\ 60.5 \end{array} $	5.9 4.6 4.9 802.5 13.4 26.6
Depth (m) 1.0 4.0 8.0 12.0 outlet inlet	11/6 27.5 20.8 0.0 0.3 2.2 41.7							

Table 4.8. Total Soluble Phosphorus ( $\mu$ g/L) in Lake Hamilton, 1987:

Depth (m)	3/27	4/09	4/23	4/30	5/08	5/15	5/21	5/28
1.0 4.0 5.0 6.0 8.0 12.0 outlet inlet	17.6 0 11.9 11.6 13.1	18.2 0 11.8 14.2 13.1	16.3 11.5 - 17.3 10.5	14.8 12.9 - 18.2 10.8	15.6 11.6 - 10.2 33.9 - 11.6	5.5 6.5 - 3.7 21.0 - 22.7	16.8 12.3 - 8.5 39.3 18.4 -	21.3 13.4  23.9 62.7  56.1
Depth (m)	6/04	6/12	6/17	6/23	7/02	7/07	7/14	7/21
1.0 4.0 8.0 12.0 outlet inlet	31.4 142.6 6.9 119.4 16.9	23.5 14.5 7.7 168.0 52.4	37.6 17.7 6.6 212.4 51.3 72.1	$     18.9 \\     14.2 \\     34.5 \\     168.6 \\     9.5 \\     102.2 $	21.2 17.2 14.8 74.0 81.6	30.6 15.9 45.8 218.1 26.6 23.0	18.3 9.3 48.2 549.9 14.5 68.4	31.4 13.5 76.4 544.9 16.8 21.6
Depth (m)	7/27	8/04	<u>8/10</u>	8/21	<u>9/01</u>	9/16	<u>9/30</u>	10/16
1.0 4.0 8.0 12.0 outlet inlet	16.6 11.7 96.3 562.1 21.3 31.5	36.4 27.1 88.9 550.5 38.3 105.4	21.1 15.0 122.2 608.5 12.3 62.7	34.9 13.4 170.0 619.0 33.8 49.3	11.5 14.5 258.9 183.1 14.6 72.1	16.7 11.9 173.2 684.1 28.9 59.7	15.4 10.6 10.1 641.6 48.2 70.0	20.0 20.6 33.7 814.5 21.8 34.7

Table 4.9. Total Phosphorus ( $\mu$ g/L) in Lake Hamilton, 1987:

<u>Depth (m)</u>	3/27	4/09	4/23	4/30	5/08	5/15	5/21	5/28
1.0 4.0 5.0 6.0 8.0 12.0 outlet inlet	60.9 	84.3 - 45.9 57.1 57.7	44.8 56.1 - 49.7 41.1	58.8 47.2 - 47.6 44.3 -	47.0 51.9 - 29.3 56.6 - 47.1	13.9 47.2 - 13.9 38.0 - 127.0	31.9 60.2 - 26.7 112.4 47.7	25.2 38.5 - 36.8 117.2 - 219.7
Depth (m)	6/04	<u>6/12</u>	6/17	<u>6/23</u>	7/02	7/07	7/14	7/21
1.0 4.0 8.0 12.0 outlet inlet	27.2 24.5 29.3 152.2 29.6	30.8 24.8 29.3 187.8 - 93.2	46.1 45.9 44.0 245.4 75.6 89.6	33.7 44.5 58.8 204.0 37.6 126.4	72:7 89.1 33.4 86.8	107.3 47.4 67.2 240.7 90.2 54.9	42.7 29.6 74.7 560.8 60.4 166.1	41.0 72.1 84.9 548.9 24.5 36.2
Depth (m)	7/27	8/04	8/10	8/21	<u>9/01</u>	<u>9/16</u>	<u>9/30</u>	10/16
1.0 4.0 8.0 12.0 outlet inlet	34.0 83.4 128.4 603.2 29.8 41.6	50.3 113.0 122.9 826.8 52.3 113.8	59.0 56.1 127.8 574.8 74.0 88.3	51.0 86.1 183.8 625.3 31.7 59.6	63.1 40.7 168.1 247.2 61.8 115.6	41.2 25.7 191.2 616.3 28.9 59.7	41.8 31.4 47.4 667.8 61.5 78.9	149.4 53.8 64.4 814.5 29.4 40.0
Depth (m)	1	1/6						
1.0 4.0 8.0 12.0 outlet inlet	5 7 7 8 2 6	7.4 9.2 9.7 6.0 4.7 7.5						

<u>Depth (m)</u>	3/27	4/09	4/23	4/30	5/08	5/15	5/21	5/28
1.0 4.0 5.0 6.0 8.0 12.0 outlet inlet	2.1  19.8  6.87 	11.5 - 14.9 12.6	25.34 19.73 - 9.62 -	16.95 10.32 - 7.32 -	14.73 13.53 - 2.71 4.61 -	7.42 27.21  2.66 3.86 	4.01 32.98 - 3.01 2.61 -	0.65 6.36 - 4.11 3.36 -
Depth (m)	6/04	6/12	6/17	6/23	7/02	7/07	7/14	7/21
1.0 4.0 8.0 12.0 outlet inlet	3.21 3.91 5.11 3.11 -	5.31 7.72 8.42 3.41 -	4.91 9.72 14.13 4.81 -	29.87 14.33 6.11 3.81 -	47.11 17.91 4.81 3.91 -	79.66 4.41 2.1 2.21 -	10.32 8.12 3.31 5.31 -	7.62 64.55 2.81 3.01
<u>Depth (m)</u>	7/27	8/04	8/10	8/21	9/01	9/16	<u>9/30</u>	10/16
1.0 4.0 8.0 12.0 outlet inlet	13.23 62.15 3.51 3.91 -	26.36 18.04 4.01 4.31 -	58.34 4.94 3.31 3.41 -	7.9 2.8 1.9 3	17.22 8.9 1 0.8 -	19.72 2 0.7 0.74 -	19.6 6 12 1.4 -	9.4 6 0.7 0.9 -

Depth (m)	11/6
1.0	1.5
4.0	0.7
8.0	1.6
12.0	0.8
outlet	-
inlet	-

Depth (m)	<u>3/27</u>	4/9	4/23	4/30	5/8	5/15	5/21
1 4 12 outlet inlet		1087.5 - 399.3 522.1 -	0 - 318.9 -	201.8 - - 196.7 -	77.7 228.6 499.5 294.8 - 57.3	42.6 98.2 459.9 248.2 - 647.8	737.7 81.8 397.0 213.5 157.9
Depth (m)	5/28	6/4	6/12	6/17	6/23	<u>6/30</u>	7/2
1 4 12 outlet inlet	199.1 10.9 360.7 185.1 - 559.7	258.1 16.3 349.9 87.4 242.6	268.0 63.0 42.9 625.8	189.3 182.1 64.7 8.2 197.1 454.9	81.4 147.2 - 39.2 760.2 48.1	219.9 58.6 1077.8	
Depth (m)	7/7	7/14	7/21	7/27	8/4	8/10	8/21
1 4 8 12 outlet inlet	973.2 1065.6 - - 846.1 710.1	446.9 509.6 21.2 - 427.4 567.3	529.9 775.8 - 92.3 243.5	362.9 407.1 - 143.6 461.5	- 243.3 - - 54.6	9.1 80.0 - - 630.5	35.2 - - 88.5 118.0
<u>Depth (m)</u>	9/1	9/16	<u>9/13</u>				
1 4 12 outlet inlet	415.	- - 117. - 9. - 7 574.	- 9 4. 5 - 103. 6 33	- 2 - 5 3			

Depth (m)	3/27	4/9	4/23	4/30	5/8	5/15	5/21
1 4 8 12 outlet inlet		9.2 - 372.2 16.8	11.6 - - 11.9 -	20.4 - 393.0 19.4 -	5.6 55.2 175.3 721.5 - 2.6	9.5 11.0 191.5 656.2 - 85.1	54.8 0.1 186.7 745.7 40.1
Depth (m)	5/28	6/4	6/12	6/17	6/23	<u>6/30</u>	7/2
1 4 8 12 outlet inlet	14.5 212.3 769.1 102.2	43.8 9.5 258.4 934.9 66.8	29.1 11.1 232.7 962.1 - 55.1	34.0 80.2 268.4 1635.6 433.6 102.3	14.5 85.5 451.0 1149.5 9.5 104.8	13.5 21.7 112.5 721.5 - 160.2	
Depth (m)	7/7	7/14	7/21	7/27	8/4	8/10	8/21
1 4 8 12 outlet inlet	7.2 121.5 274.5 1034.4 21 -	48.3 171.0 347.1 1944.6 - 68.5	22.6 14.2 404.2 1790.8 118.5 17.0	3.1 523.8 1826.3 113.9 0.2	20.2 124.8 621.3 2546.9 27.2 31.3	9.9 157.0 417.9 1711.8 11.1 -	31.0 2.0 537.8 844.0 113.4 22.0
<u>Depth (m)</u>	9	/1 9/	16 9/	30			
1 4 8 12 outlet inlet	56 68 1330 1163 40 620	.7 4 .4 253 .7 1157 .7 2346 .8 44 .7 20	.5 78 .1 28 .9 26 .7 2738 .1 288 .1 17	.8 .7 .4 .2 .9 .4			

06/23

Depth (m)	Temp. <u>°C</u>	D.O. mg/L	SRP µg/L	TP µg/L	TSP µg/L	Chl <u>a</u> µg/L
$\begin{array}{c} 0.5 \\ 1.0 \\ 1.5 \\ 2.0 \\ 2.5 \\ 3.0 \\ 3.5 \\ 4.0 \end{array}$	24.4 24.2 24.2 24.1 23.5 22.0 21.0 18.7	12.0 11.9 11.3 10.7 7.3 3.9 1.8 2.2	3.6	42.4	11.8	33.3 - - 6.7
07/07						
Depth (m)	Temp. <u>°C</u>	D.O. <u>mg/L</u>	SRP <u>µg/l</u>	TP µg/L	TSP <u>µg/L</u>	Chl <u>a</u> µg/L
$\begin{array}{c} 0.5 \\ 1.0 \\ 1.5 \\ 2.0 \\ 2.5 \\ 3.0 \\ 3.5 \\ 4.0 \end{array}$	24.8 23.7 22.5 21.3 20.2 20.0 19.8 19.8	15.4 14.0 11.4 7.8 4.7 4.4 4.0 2.8	4.0	71.5	11.8 - - 11.8 -	24.9 - - 6.9 -
07/27						
Depth (m)	Temp. <u>°C</u>	D.O. mg/L	SRP <u>µg/l</u>	TP µg/L	TSP µg/L	Chl <u>a</u> µg/L
0.5 1.0 1.5 2.0 2.5 3.0 3.5	26.2 26.1 26.0 26.0 26.0 24.5 22.5	12.1 11.6 11.3 11.2 10.9 5.5 3.4	0.8	- 54.2 - - 96.6	- 17.3 - - 15.4 -	43.8

Table 4.14. Volume-Weighted Average Concentrations for Lake

Hamilton, 1987 (provided by Kotwal, 1992)

VOLUME WEIGHTED AVERAG	E CONCENTRATIONS I	FOR LAKE HAMILTON: 1987
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JULIAN	DATE	DO(PPM	)	PO4(PP	8)	OP(PPB	)	TP(PPB	9	CHLa(P	PB)	NH3(PP	8)	NO3(PPB) ON(PP		PPB)	
DAY		EPI.	HYPO	EPI.	HYPO	EPI.	HYPO.	EPI.	HYPO	EPI.	HYPO.	EPI.	HYPO	EPI.	HYPO.	EPI.	HYPO.
0	12/31/86	11.35	8.35	14.98	13.68	49 26	47.2	64.22	60.88	107	4 13	10	70	460	430	1000	95
86	3/27	13 8	93	3.95	2.09	49 97	41 28	53.92	43 37	20 63	14 99						
99	4/9	117	86	3 12	1.53	69 38	48.53	725	50 08	12 55	14 04	92	284 24	1087.5	566.08		
113	4/23	13.1	7	2.42	1.87	48 87	51.45	49 29	53 32	23 11	153	116	11.6	0	241.63		
120	4/30	112	6	3.4	28	50 79	44 57	54 19	47.37	14 31	9 02	20.4	302 71	201.8	201.8		
128	5/8	11.5	48	18	3.52	47.61	35 8	49 41	39 32	14 14	4.59	29 97	302 72	151 85	411.42		
135	5/15	10 4	2.4	2.11	4 49	28.15	19 96	30 26	24 45	17.14	6 11	10 24	289 91	69 92	358.41		
141	5/21	81	2	3.58	9.73	42 23	43 64	45.81	53 37	18 24	673	27 92	308 97	415 42	308 81		
148	5/28	93	1	5.58	19 34	26 18	38 69	31 74	58 03	3 46	42	7 38	330 72	106 63	270 16		
155	6/4	91	13	3 15	30 57	22.72	30 24	25 87	60 81	3 55	4 43	26 95	403 43	139 29	238 72		
163	6/12	10.7	1.7	3 02	41 22	24.83	28.93	27 85	70.15	8 49	7 02	20 26	395 04	167.27	52 94		
168	6/17	98	16	321	52 38	42.79	44 5	48	96 88	7 27	11 13	56 7	601 69	185 78	64 92		
174	8/23	8.3	17	301	67 12	36	27.8	39 01	94 92	22 23	6 56	49.39	586 9	113.73	29.03		2111
183	7/2	68	1.7	491	21 41	75 85	33 06	80 76	54 47	32.76	6 25				1		
188	1/7	92	07	803	75 48	69 84	34.54	77.87	110 02	42 69	2 42	63 36	453 57	1018 8	136 02		
195	7/14	6	0.3	2.11	153 28	34.15	42.7	36 28	195 98	924	4 45	108 59	742 12	477.71	78		
202	7/21	66	0.04	2 07	176 01	54 21	28 52	56 28	204 53	35 59	10 74	18 47	716 8	650 72	99 02		
208	7/27	7 95	0	078	183 45	57 51	63 29	58 27	246 74	37.27	11.1	1 58	797 34	384 62	51 96		
216	8/4	9 68	0	1 79	183 22	79 32	122 38	81.11	305 6	22 27	5 88	716	1061.17	119 55	31 08		
222	8/10	4 88	0	4 34	174.86	53 24	60 61	57 58	235 47	32.1	3.54	82 18	722 75	43 94	10 21		
233	8/21	6.7	0	0	2182	68 25	68 51	68.25	286 71	5 39	23	16 75	549 43	179	0		
244	9/1	7 51	0	0	163 38	52 09	70 23	52 09	233 61	13 13	1 96	62 45	1125 93	0	0		
259	9/16	7 22	0	075	225 54	32 83	55 63	33 58	281 17	1101	0 88	126 65	1353 09	87 41	25 19		-
273	9/30	10 82	0 86	1 06	171 46	35 63	36 04	36 69	207 5	12 92	8 46	54 18	735 5	2 06	0 54		
289	10/16	9 26	5 98	5 26	213 31	97 17	45 77	102 43	259 08	7 73	1 43						
310	11/6	10 86	9 99	24 21	273	439	78 55	68.11	81 28	1.11	1.28						



Hamilton, 1987.

Lake Hamilton D.O. Profiles - 1987



Figure 4.3. Selected Dissolved Oxygen Profiles for Lake Hamilton, 1987.









# Figure 4.5. Secchi Depth versus time profile for Lake Hamilton, 1987.

#### 4.3 Application of Dillon & Rigler Desk Method

Dillon and Rigler (1975) developed a simple procedure for estimating the capacity for development in a watershed based on trophic status. This provides much useful information on hydrology, phosphorus loading, and predicted water quality. The step-by-step procedure is applied to Lake Hamilton below.

1. Lake Morphometry

From Hypsographic Curve (Table 4.1)

a. Lake surface area (Ao in  $m^2$ )

 $A_0 = 2,419,244 + 1,855,663$ 

 $= 4,274,907 \, \mathrm{ft}^2$ 

 $= 4,274,907 \times (.3048)^2$ 

 $= 397.151.68 \text{ m}^2$ 

b. Lake's total volume (V in m<sup>3</sup>) (Table 4.1)

V = 1/2 (2,419,244 + 1,866,410) <u>10</u> + 1/2 (1,866,410 + 783,809)10

+ 1/2 (783,889)5 + 1/2 (1,855,663 + 1,783,123)10

+ 1/2 (1,783,123 + 1,577,903)10 + 1/2 (1,577,903 +

1,173,972)10

+ 1/2 (1,173,972 + 448,467) 10 + 1/2 (448,467 + 133,300) 10

+ 1/2 (133, 300) 5

= 96,752,202.5 ft<sup>3</sup>

 $= 96,752,202.5 \times (0.3048)^3$ 

 $= 2,739,717.28 \text{ m}^3$ 

- c. Mean Depth (Z in m)
- $Z = \frac{2,739,717.28 \text{ m}^3}{397,1515.86 \text{ m}^2} = \frac{6.9 \text{ m}}{2}$

2. Drainage area Ad was calculated on a 1:50,000 scale topographic map (Figure 4.6), and was found to be,  $A_d =$ 27,111,334 ft<sup>2</sup> (by Planimetry) = 27,111,334 x (.3048)<sup>2</sup> = 2,518,725.3 m<sup>2</sup>. The underlying geology of the region is of sedimentary origin.

The watershed areas dedicated to various land uses are as follows:

Pasture = 5,938,476 ft<sup>2</sup> = 551,702.44 m<sup>2</sup> Urban = 21,172,858 ft<sup>2</sup> = 1,967,022.8 m<sup>2</sup>

3. <u>Calculating outflows from the lake</u>. To find the total outflow, Q, we neglect the effect of precipitation and evaporation, and then the outflow is calculated by adding up the averages of annual flow over spillway, and output to industrial systems for the years 1983, 1984.

Then the flushing rate (P) is calculated by dividing the total flow by the total volume of the lake.

$$P = \frac{2.50 \times 10^7 \text{ m}^3/\text{yr}}{2,739,717.28 \text{ m}^3}$$

$$P = 9.13/\text{yr}$$



Figure 4.6 Local Drainage Basin of Lake Hamilton

#### 4. Areal water load

 $q_{s} = \frac{2.50 \times 10^{7} \text{ m}^{3}/\text{yr}}{397,151.86}$ 

= 62.95 m/yr

5. Phosphorous Retention coefficient (Rp) (Kirchner and Dillon 1975)  $R = 0.426 \exp (-0.271 q_s) + 0.574 \exp (-0.00949 q_s)$ where  $q_s$  (areal water load for Lake Hamilton) = 62.95

m/yr.

 $R = 0.426 \exp (0.271 \times 62.95) + 0.574 \exp (-0.00949 \times 62.95)$  $= 0.426 \exp (-17.059) + 0.574 \exp (-0.597)$  $= (1.663 \times 10^{-8}) + 0.316$ R = 0.316

Or, from Chapra (1975)

$$R_p = \frac{v}{v + q_s}$$

where v = the total apparent settling velocity of Tp = 13.2 m/y (Dillon and Kirchner 1975).

 $q_s$  = areal water loading

= 62.95 m/yr.

Then  $R_p = \frac{13.2}{13.2 + 62.95} = \frac{13.2}{76.15}$ = 0.173

and the range of R values based on this equation  $Rp_{min} = \frac{10}{10+62.95} = 0.137$  (v from Vollenweider 1975)

 $Rp_{max} = \frac{16}{16+62.95} = 0.203$  (v from Chapra 1975)

 <u>Response time</u>: This is the time for the lake to respond to a change in phosphorous loading.

Response Time = 5 (0.69)  $\rho$ = flushing rate, 1/year  $\rho + 10/Z$  Z = lake mean depth, m 5 (0.69)9.13 yr-1 + 10/6.9 m = 0.326 yr

Predicted response time to a change in P is short.

This is a good argument for the validity of a steady state model.

#### 7. Phosphorous Transport from watershed:

The area of the drainage basin, not including the lake is  $A_d = 27,11,334$  ft<sup>2</sup> = 2,518,725.3 m<sup>2</sup>; the drainage basin  $A_d$  was divided into two areas depending on various land use as follows:

Pasture = 5,938,476 ft<sup>2</sup> = 551,702.44 m<sup>2</sup>

Urban = 21,172,858 ft = 1,967,022.8 m<sup>2</sup>

The phosphorus export coefficient is estimated from Dillon and Kirchner (1975) as follows, depending on land use. Urban Land P. export coef =  $200 \text{ mg/m}^2/\text{yr}$ Pasture Land P. export coef =  $23.3 \text{ mg/m}^2/\text{yr}$ 

Then the total phosphorus loading directly from the watershed per year is calculated as follows:

 $J_{w} = 10^{-6} [(551,702.44 \times 23.3) + (1,967,022.8 \times 200)]$ = 10^{-6} (12.854667 + 3.934 × 10<sup>8</sup>)  $J_{w} = 406.25 \text{ kg/yr}.$ 

8. Total Supply of Phosphorus per year:

Mean of 21 measurements of TP in Yellow Cr. inlet was 83.2 ug/L, or 0.0832g/m<sup>3</sup>, so the estimated loading is:

.0832 g/m<sup>3</sup> x 10  $^{-3}$ kg/g x 2.50 x 10<sup>7</sup> m<sup>3</sup>/yr  $J_{yc} = 2087.5$  Kg/yr Phosphorus loading due to precipitation is estimated as:  $J_{pr} = \frac{75}{10^6}$  A0 =  $\frac{75 \times 397.151.68}{10^6}$  = 29.79 kg/yr  $J_{tot} = 2087.5 + 406.25 + 29.79$   $J_{tot} = 2523.54$  kg/yr Then the areal phosphorus loading per year into the lake is:  $L = \frac{J_{tot}}{10^6}$ 

Ao

 $L = 2523.54 = 0.0063541 \text{ kg m}^{-2} \text{ yr}^{-1}$ 397,151.86

 $L = 6354.1 \text{ mg m}^{-2} \text{ yr}^{-1}$ 

9. <u>Predicted Water Ouality</u> from Dillon & Rigler (1974): [TP] =  $\frac{L (1-R)}{Z \times \rho}$ 

Flushing Rate (Lake Hamilton) =  $8.79 \text{ yr}^{-1}$ 

Z = 6.90 m

 $R_1 = 0.316$  yr by Kirchner & Dillon (1975) equation

 $R_2 = 0.173$  yr by Chapra (1975) equation and Dillon and Kirchner (1975) value of v.

 $\rho = 9.13/yr$ 

Performing calculations for both retention coefficients:

$$[TP_1] = \frac{6354.1 (1 - 0.316)}{6.9 \times 9.13} = \frac{4346.20}{63.00} = 68.99 \text{ mg/m}^3$$
$$= 68.99 \text{ µg/L}$$
$$[TP_2] = \frac{6354.1 (1 - 0.173)}{6.9 \times 9.13} = \frac{5254.84}{63.00} = 83.41 \text{ mg/m}^3$$

 $[TP_2] = 83.41 \ \mu g/L$ 

Predicted chlorophyll a and secchi depth:

For 
$$[TP_1] = 68.99 \ \mu g/L$$
 (from  $R_1 = 0.316$ )  
 $Log_{10} \ [chla]_1 = 1.45 \ Log_{10} \ [TP] - 1.14$   
and  $[chla]_1 = 33.69 \ mg/m^3$   
 $SD_1 = 48 = 48 = 0.70 \ m$   
 $[TP_1] \ 68.99$   
 $TP_2 = 83.41 \ (from R_2 = 0.173)$   
and  $[chla]_2 = 44.24 \ mg/m^3$ 

 $SD_2 = \underline{48} = \underline{48} = 0.58 \text{ m}$ [TP<sub>2</sub>] 83.41

#### Comparison with Field Data

If we use the spring turnover values from our actual data we get 50 mg/L for an average total phosphorus value, so both  $TP_1 \& TP_2$  were high. Then from the actual data, and from the months of June, July and August we get

Actual  $chl_{ave} = 21.4 \text{ mg/m}^3$  (n = 12)

using the volume weighted average in the epilimnion

Actual  $SD_{ave} = 2.53 \text{ m}$  (n = 12)

by Dillon & Rigler Eqn. assuming L is correct

$$[TP] = \frac{L (1 - R)}{Z \times \rho}$$
for  $[TP] = 50 \ \mu g/L = 50 \ m g/m^3$ 

$$50 = \frac{6354.1 (1-R)}{6.9 \times 9.13} = \frac{6354.1 - 6354.1R}{63.00}$$

$$3149.85 - 6354.1 = -6354.1R$$

$$R = 0.504$$
Calculating L required to reduce  $[TP]$  to 20  $\mu g/L$  (mesotrophic status) using this value of R:  

$$L = \frac{Z \times \rho \times [TP]}{1 - R} = \frac{6.9 \times 9.13 \times 20}{1 - 0.504} = 2540.22 \ \text{mg} \ \text{m}^{-2} \ \text{yr}^{-1}$$
or  $J_{\text{tot}} = 1008.9 \ \text{kg/yr}$ 

## 4.4 Application of Vollenweider Loading Plot

Dillon and Rigler's "Desk Method" is one way to evaluate lake trophic status. Another way is using a phosphorus loading plot, like the one developed by Vollenweider (1975). By plotting the areal total phosphorus loading rate versus depth divided by hydraulic residence time for a large number of lakes, Vollenweider was able to identify regions corresponding to each trophic status classification. The trophic status of a lake can be estimated by finding its plotting position on these axes and comparing this position to the region boundaries.

For Lake Hamilton  $\frac{Z}{L} = \frac{6.9 \text{ m}}{0.11 \text{ yr}} = 62.7 \text{ m/yr}$   $L = \frac{J}{A} = 6.35 \text{ g/m}^2/\text{yr}$ 

The location of Lake Hamilton on the Vollenweider (1975) plot is shown in Figure 4.7. This plot suggests that the lake is highly eutrophic, which is consistent with the field data.



Figure 4.7 Lake Hamilton Trophic Status Prediction Using Vollenweider's (1975) Loading Plot

#### Chapter Five

Summary, Conclusions and Recommendations

#### 5.1 <u>Conclusions</u>

- A. Lake Hamilton in Struthers, Ohio, was sampled and analyzed in this study, and the lake was classified to be highly eutrophic using the phosphorus loading plot of Vollenweider (1975).
- B. Much of the data required for application of a more detailed mechanistic model has been collected and summarized for 1987.
- C. Calculations were performed for many important hydrologic and morphometric parameters.
- D. The total phosphorus loading was estimated to be 2523 kg/yr, or 6354 mg/m<sup>2</sup>/yr, by the [Dillon and Rigler (1975) "desk method"]. For Lake Hamilton to return to mesotrophic status, a reduction in phosphorus loading to 1000 kg, or 2540 mg m<sup>-2</sup> yr<sup>-1</sup>, yr

(a 60% reduction) is required.

E. Concentrations of total phosphorus (TP) predicted for Lake Hamilton using the procedure of Dillon and Rigler (1975) were higher than the average concentration actually measured in the lake during 1987. Using the average measured TP from 1987 field

data, the phosphorus retention coefficient (R) was estimated to be 0.504.

#### 5.2 <u>Recommendations</u>

- A. To gain more insight into processes in Lake Hamilton, data collected in this study should be used to apply more detailed mechanistic models of lake trophic status.
- B. The current estimate of total phosphorus (TP) loading to Lake Hamilton is very crude. Before evaluating different lake management strategies for controlling eutrophication, a more accurate estimate of TP loading is needed. This would require gauging of flows into Lake Hamilton from Yellow Creek and routine monitoring of TP concentrations.

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